

Metallurgy for Industries

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ARTiS

Integrated Approach for RLA of Reformer Tubes by NDT

The primary reformers / hydrogen crackers are widely used in fertilizers, petrochemicals and refining industries. They produce hydrogen by endothermic reaction at elevated temperature above 800°C in pressurized condition. Challenge to combat creep and thermal damages for long term durability has catapulted research in alloy development. There had been continuous development in satisfactory design of tubes to generally achieve operating life in excess of 100,000 hours. The tube replacement strategy is dependent on NDT inspection results. Various inspection methods are deployed in isolation and judgments are taken predominantly based on past experience of the end user.

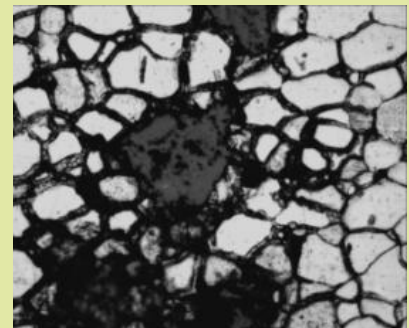
Normally decisive factors for tube replacement are: (a) increase of diameter in the range of 3-6% is considered a limiting creep strain. (b) More than 65 dB of ultrasonic attenuation signals warning about creep fissure detection on vis-a-vis tube bowing and overall service life – if it exceeds sufficient operating hours it may call for tube replacement.

The integrated approach of reformer tube inspection by ARTiS – can provide correlation between tube metallurgy and inspection findings. Comprehensive approach for tube retirement plan based on combination of NDT inspection and metallographic techniques is arrived through ARTiS.

ARTiS is abbreviated form for “Automated Reformer Tube Inspection System”. This is a robotic crawler that maneuvers ultrasound scanning of reformer tubes in a more systematic manner and provide tabular output. The method imbibes same principle of manual scanning widely accepted by the industry with necessary improvements. During scanning, ARTiS provides attenuation (dB level), diameter wise throughout the length of the tube, having a specially installed electronic device for trajectory detection; it also provides bowing of the tube.

The inspection output thereby becomes more categorical and traceable throughout the tube height. ARTiS avoids the need of scaffolding and saves inspection time, achieving reduced shutdown of plant. Comparison between ultrasonic inspection by

Microstructure of the Month



Magnification: 400X

Component: Super-heater coil

MOC: SA-213 T22

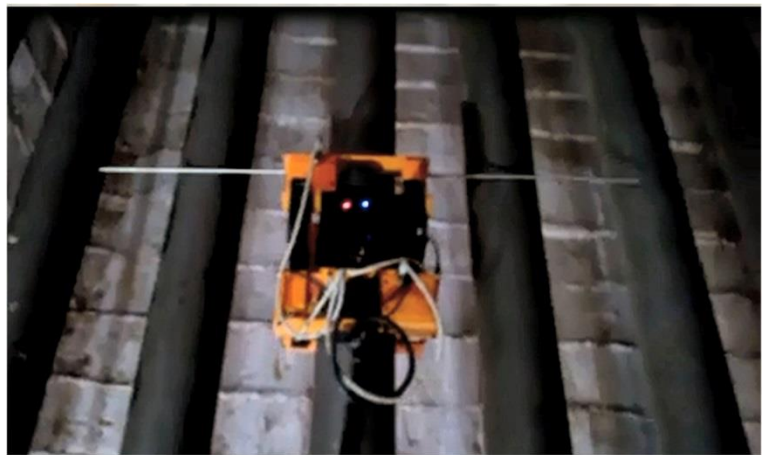
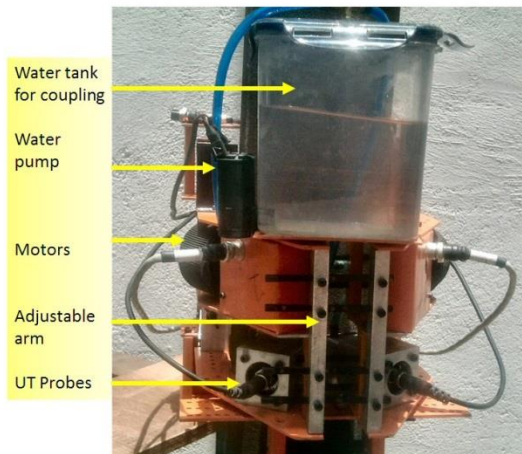
Observation: Microstructure shows view of OD surface having inter granular cracking with sulphidation/oxidation observed at the cracks.

Cause: The failure noticed in the super heater coil is due to the long term overheating leading to high temperature sulphur induced corrosion, preferentially attacking the grain boundaries, which is essentially due to localized increase in temperature in view of higher scaling at ID and presence of sulphur from the flue gases.

Useful Hint: OD surface conditions should be monitored by in-situ metallography and hardness to foresee any metallurgical degradation. Degraded coils may be replaced. Thickness measurement on tubes surface after removal of oxide scale. Tubes may be replaced based on thickness criteria. RLA of the super heater coils may be carried out to work out for long term remedial actions.

manual method and by ARTiS is given in table below.

| Parameter | Manual method | ARTiS |
|---|---|---|
| Requirement of scaffolding | Needed | Not needed |
| Cost of scaffolding | At actual | Nil |
| Time required for erection and removal of scaffolding | 1 to 2 days | Nil |
| Requirement of D.M. water | Continuous | Limited |
| Spillage and wetting of surrounding during test | Uncontrolled | Nil |
| Time of test (3 persons team) | 3 to 5 days for 100 tubes | 2 to 3 days for 100 tubes |
| Resolution of test result | 1.5 - 2.0 meters | 0.1 meter |
| Outer diameter measurement | One or two locations manually | Every 0.1 meter |
| Tube bowing | Qualitative judgment or by plumb measurement, additional time | Quantitative measure during UT scan |
| Safety consideration | Higher risk (elevated work area) | Lower risk (platform area) |
| Reporting | Manual data entry | Software based with statistical data analysis |



Based on TCR's past experience of inspection, failure investigations of reformer tubes and life assessment studies, correlation is made with NDT results to arrive at an ageing mechanism. The tube condition indexing is described in following table.

| Test | Index[1] (higher is worse) | | | |
|----------------------------|---|--|--|--|
| | 0 (least aged) | 1 | 2 | 3 (most aged) |
| General visual examination | Good condition with no significant abnormality. | Apparent change in weld or apparent offset or abnormal coloration | Apparent localized bulging or shiny surface | Presence of crack, bulged with craze pattern |
| Visual baldness | Good surface roughness | Smooth surface texture on touch and feel | - | - |
| Bowing of tubes | < 0.1X of tube diameter | Up to 0.5X of tube diameter | Up to 0.8X of tube diameter | Up to 1X tube diameter |
| Ultrasonic attenuation[2] | Up to 50 db | Up to 58 db | Up to 70 db | > 70 db |
| Creep strain | < 2% | 2 to 3 % | 3 to 5 % | > 5% |
| Microstructural condition | Microstructure without any significant grain coarsening | Dilation of secondary carbides towards grain boundary with coarsening of primary grain boundary carbides | Presence of isolated or oriented creep voids preferably normal to principle stress direction | Presence of interconnected, parallel micro cracks normal to principle stress direction |
| Overall index | Sum of individual indexing | | | |

Notes:

[1] Proprietary index weightage factor is not shown. Remaining tube life as per API530 is separately addressed by thickness measurement, outer diameter value and microstructural condition.

[2] Value is indicative, dependent on instrument settings, surface roughness of tube, test equipment and coupling conditions.

Conclusion: The non-destructive testing of reformer heater tubes places undue emphasis predominantly on ultrasonic attenuation measurements. However, change in microstructural condition such as carbide coarsening, secondary carbide precipitation and depletion / dissolution of carbides from the grains, largely affect the ultrasound attenuation mechanism. Only conditions like complete loss of ultrasound energy can indicate presence of mid-wall fissures, which still requires confirmation by alternate NDT- like radiography.

The tube life assessment based only on NDT approach has so far remained in isolation, and it can only be improved by comprehensive tube inspection covering not only NDT but also techniques like ARTIS and metallography.

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